

Catalysis Today 30 (1996) 163-170



# Novel oxygen storage components for advanced catalysts for emission control in natural gas fueled vehicles

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#### Abstract

Advanced catalysts based on a novel oxygen storage component (OSC) were developed for emission control in natural gas fueled vehicles. The catalysts contain a manganese oxide  $(MnO_x)$  as the OSC supported on an inert LaAlO<sub>3</sub> perovskite and a noble metal component (Pd) supported on a separate high surface area refractory material, for example lanthana stabilized  $Al_2O_3$ . The  $MnO_x$  has higher oxygen storage capacity, and faster oxygen absorption and oxide reduction rates than the present commercial ceria-stabilized alumina support materials. Temperature programmed techniques and dynamic cycled experiments were used to measure oxygen storage capacity, activity for NO reduction and CO and  $CH_4$  oxidation rates. Durability tests on a physical mixture of  $Pd-Mn/LaAlO_3$  and  $Pt/Al_2O_3(La)$  demonstrated that a temperature excursion to 950°C for 30 min did not cause significant loss in catalyst activity for either NO reduction or CO or  $CH_4$  oxidation. We have also shown that the  $MnO_x$  can be added to conventional three-way catalysts (TWC) to enhance their performance for  $NO_x$  reduction and CO or hydrocarbon oxidation.

Keywords: High temperature three-way catalyst (TWC); Oxygen storage component (OSC); Emission control for natural gas fueled vehicles; Manganese oxide  $(MnO_x)$ 

#### 1. Introduction

Natural gas has received increased attention as an alternative fuel for motor vehicles because of its potential technical, economic, and environmental advantages. Natural gas vehicles (NGV) generate exhaust gas with extremely low photochemical reactivity [1], produce low coldstart CO emission [2], and have zero evaporative emission. On the other hand, NO<sub>x</sub> emissions as well as CO and unburned CH<sub>4</sub> (a much more powerful greenhouse gas than CO<sub>2</sub> [3,4]) in NGV exhaust need to be greatly reduced. Conventional three-way catalysts (TWC) currently used for gasoline-vehicle exhaust emission control showed poor methane conversion

for NGV exhaust gas [5]. Therefore, new catalyst formulations are needed to reduce levels of these pollutants in NGV exhaust to meet ultralow emission vehicle (ULEV) standard.

Conventional TWC presently used in automobile catalytic converters work well for reducing CO, hydrocarbons (HCs), and  $NO_x$  emissions in strict stoichiometric combustion exhaust. However, most pollution (80%) is produced under conditions outside the stoichiometric window. Therefore, to meet the new stringent emission standards, particularly, the ULEV standards, catalysts which function in a wider air-to-fuel ratio range must be developed. They must be able to supply oxygen to oxidize CO and HCs when exhaust is fuel rich and remove

excess oxygen when it is lean. The key to such catalysts is to find an OSC which has superior performance than Ce-based OSC [6,7]

The objectives of this work was to develop oxygen storage materials with higher capacity, faster oxygen absorption and oxide reduction rates than present commercial ceria supported on alumina, to find supports which have high surface area and highly sintering resistant, and to formulate catalysts to be used for high-temperature three-way emission control for natural gas fueled vehicles.

In this work, we report  $MnO_x$  as an OSC supported on a variety of highly refractory materials that can be used for  $NO_x$ ,  $CH_4$ , and CO reduction in NGV exhaust gas. Both temperature programmed and dynamic cycled techniques were developed and used to measure the oxygen storage capacity and catalytic activity for  $NO_x$ ,  $CH_4$ , and CO reduction under dynamic cycled conditions similar to that from an engine manifold.

# 2. Experimental

#### 2.1. Materials

Catalyst supports, LaAlO<sub>3</sub> perovskite, LaAl<sub>11</sub>O<sub>18</sub> (hexaaluminate), and BaAl<sub>12</sub>O<sub>19</sub> (hexaaluminate) were prepared using a sol-gel technique and supercritical drying [8] while lanthanum stabilized Al<sub>2</sub>O<sub>3</sub>(La), and BaAl<sub>2</sub>O<sub>4</sub> spinel were prepared by ball milling and impregnation procedures. 10%Ce/Al<sub>2</sub>O<sub>3</sub> was prepared by impregnation. The final calciantion temperature was 1250°C for LaAl<sub>11</sub>O<sub>18</sub>, 1025°C for LaAlO<sub>3</sub>, 1000°C for BaAl<sub>12</sub>O<sub>19</sub> and 10%Ce/Al<sub>2</sub>O<sub>3</sub>, 1100°C for Al<sub>2</sub>O<sub>3</sub>(La), and 800°C for BaAl<sub>2</sub>O<sub>4</sub>.

### 2.2. Temperature programmed experiments

Temperature programmed oxidation (TPO) in diluted oxygen, reduction (TPRd) in diluted hydrogen, and reaction (TPR) experiments were carried out in a microreactor. An amount of 0.1 g of catalyst powder was used. Reaction effluents were analyzed by an on-line quadrupole mass spectrometer (EAI).

# 2.3. Dynamic cycled experiments

Fast (~2 Hz) and slow (0.25 Hz) dynamic cycled experiments were conducted in a dynamic switched flow micro-reactor system illustrated in Fig. 1. The amount of catalyst used was 50 mg in powder form. With balanced resistance to flow (pressure drop across the microreactor bed and a by-pass metering valve) dilute oxygen and pure helium are alternately switched into net reducing mixtures for slow and fast transients.

#### 3. Results and discussion

Fig. 2 gives the X-ray diffraction pattern of 8%Mn supported on LaAlO<sub>3</sub> perovskite. The XRD characteristics are exactly the same as LaAlO<sub>3</sub> alone, indicating that the support is exclusively perovskite phase and after impregnation with Mn salt solution and calcination at 800°C does not change the support. This is also supported by BET surface area measurements

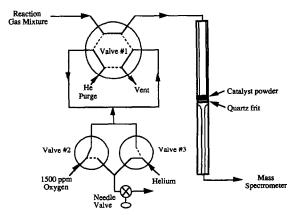


Fig. 1. Schematic diagram of the dynamic switched flow reactor apparatus used for cycling experiments. The needle valve is used to balance pressures to minimize flow bursts and the 6-port valve is used to by-pass the switched-in flow.

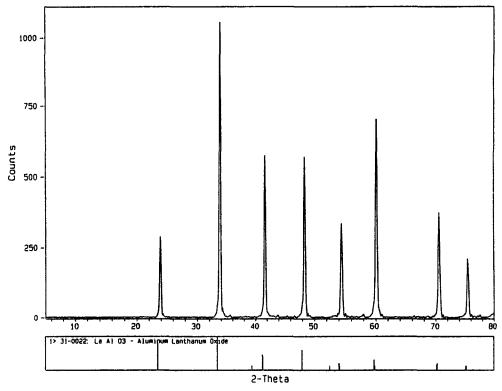


Fig. 2. XRD patterns of LaAlO<sub>3</sub> perovskite loaded with 8 wt% Mn powder sample.

(LaAlO<sub>3</sub>:  $16.2 \text{ m}^2/\text{g}$  vs.  $8\%\text{Mn/LaAlO}_3$ :  $14.7 \text{ m}^2/\text{g}$ ) that no significant surface area changes occurred after impregnation.

Table 1 presents the oxygen storage capacity of MnO<sub>x</sub> supported on a variety of supports, measured by TPO and TPRd using hydrogen. These results clearly show that Mn/LaAlO<sub>3</sub> catalysts have large OSC. Fig. 3, a typical TPO profile of supported reduced MnO<sub>x</sub> on LaAlO<sub>3</sub> perovskite, shows that MnO<sub>x</sub> has good O<sub>2</sub> up-

take (oxidation) and O<sub>2</sub> release (reduction) rates at temperatures below 600°C. This performance was confirmed by TPRd and was significantly better than that of ceria-stabilized alumina.

Irreversible formation of complex oxides (aluminates) may be the major reason for industry's past failure to develop stable emission control catalysts using first-row transition metal oxides (Mn, Fe, Co, Ni, Cu). These single metal oxides sinter rapidly when unsupported and irre-

Table 1 Temperature programmed measurements of total OSC of supported  $MnO_{\star}$ 

Catalyst	OSC by TPO $(\mu \text{mol O}_2/g_{\text{cat}})$	OSC by TPRd $(\mu \text{mol H}_2/g_{cat})$	Theoretical a ( \( \mu \text{mol O} / g_{cat} \)	
2 wt% Mn/LaAlO <sub>3</sub>	94	225	182	
4 wt% Mn/LaAlO <sub>3</sub>	114	290	364	
8 wt% Mn/LaAlO <sub>3</sub>	225	555	728	
4 wt% Mn/Al <sub>2</sub> O <sub>3</sub> (La)	81	285	364	
4 wt% Mn/BaAl <sub>12</sub> O <sub>19</sub>	66	203	364	
4 wt% Mn/silicalite	34	272	364	

<sup>&</sup>lt;sup>a</sup>  $Mn_2O_3 \rightarrow 2MnO + 1/2O_2$ .

versibly react with common alumina-based supporting oxides at moderate temperatures to form inactive aluminate spinels [9,10]. Thermochemical analysis suggests that the combination of a stable alkaline earth (e.g. Ba) or rare earth (e.g. La) oxide with alumina will yield complex oxides of sufficient stability that they cannot form aluminate oxides. We believe that no transition metal other than manganese can remain in the +2 valence state and resist reduction to the readily sintered, and difficult to re-oxidize, metallic form under rich A/F conditions nor remain in the +3 valence state under lean conditions found in a four cycle engine exhaust. High capacity for oxygen and rapid oxidation and reduction rates are possible with such a moderate valence swing.

Fig. 4 gives the typical on-line waveforms for slow and fast switch experiments conducted on a powder catalyst sample (Pd-Mn/LaAlO<sub>3</sub>) in the absence of reactions. An argon trace was used to locate the switch front as the gas mixture arrives at the downstream analyzer. Key properties determined by these experiments are the rates of reduction and reoxidation, the extent of specific oxidation and reduction of the oxide, and the mean oxygen level as functions of

temperature, average stoichiometry, and amplitude of the swing in O<sub>2</sub> partial pressure.

Due to its simplicity and its importance in emission control using TWC catalysts, the oxidation of CO by O<sub>2</sub> was chosen to measure the dynamic oxygen storage capacity. During the cycled experiments, the concentration CO was kept constant (0.3 vol%) while that of  $O_2$  was alternated between 0.05 vol% and 0.20 vol%. This was achieved by having constant 0.05 vol%  $O_2$  added to the system and adding 0.15 vol% O<sub>2</sub> from the switched-in flow. In effect, in the CO-rich half-cycle, it has net excess 0.2 vol% CO and in the O<sub>2</sub>-rich half-cycle a net excess 0.05 vol% O<sub>2</sub>. Therefore, if the catalyst does not show any oxygen storage capacity, in the O<sub>2</sub>-rich half-cycle, the level of O<sub>2</sub> breakthrough will be higher than 0.05 vol%. Levels of O<sub>2</sub> breakthrough depend on the activity of catalysts.

# 3.1. $1\%Pd-10\%Ce/Al_2O_3$

Fig. 5a gives the results of ceria (10 wt% Ce) stabilized  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> supported 1 wt% Pd for the oxidation of CO. Complete conversion of CO was achieved in the O<sub>2</sub>-rich half-cycle at  $\geq$ 

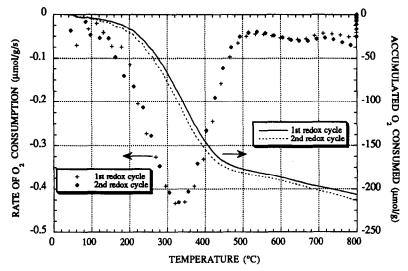


Fig. 3. TPO profile of the LaAlO<sub>3</sub> perovskite supported reduced MnO<sub>x</sub> (8 wt% Mn) catalyst by 1 vol% O<sub>2</sub> in He; flow rate: 40 cm<sup>3</sup>/min; catalyst mass: 0.1 g; heating rate: 30°C/min.

350°C. This catalyst is much more active than the supported  $MnO_x$  catalysts. At temperatures above 350°C, levels of  $O_2$  breakthrough decrease with increase of temperature. The levels of  $O_2$  breakthrough at  $\geq 350$ °C are below 0.05 vol%. However, no complete removal of  $O_2$  was achieved. The level of  $O_2$  breakthrough at high temperatures is significantly higher than  $LaAlO_3$  or  $La_2O_3$  stabilized  $\gamma$ - $Al_2O_3$  supported  $MnO_x$  at the corresponding temperatures, suggesting that this catalyst has lower OSC than 8 wt%-Mn/LaAlO3 and 8 wt%-Mn/Al2O3(La). The low oxygen storage capacity of 1%Pd-10%Ce/Al2O3 is due to ceria not because of the  $\gamma$ -Al2O3 support since 1 wt% Pd and 10

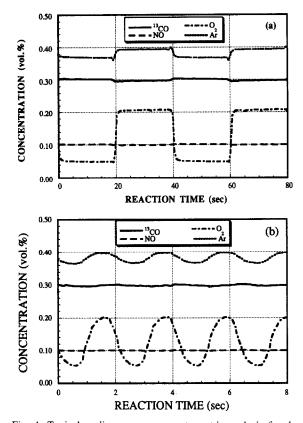
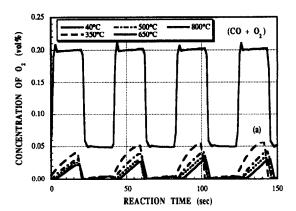


Fig. 4. Typical on-line gas mass spectrometric analysis for the dynamic switched flow reactor showing composition waveform in the absence of reaction. 20 mg of 1 wt% Pd and 8 wt% Mn supported on LaAlO<sub>3</sub>; reactant gas composition, 0.3 vol% CO, 0.05 (reducing) and 0.2 (oxidizing) vol%  $O_2$  with 0.36 vol% (reducing) and 0.40 vol% (oxidizing) Ar tracer in He; total flow,  $100 \text{ cm}^3(\text{NTP})/\text{min}$ ; (a) half cycle time, 20 s; (b) half cycle time, 1 s; GHSV:  $600000 \text{ h}^{-1}$ .



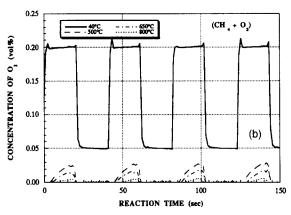


Fig. 5. Dynamic slow cycle redox reactions of CO and CH<sub>4</sub> with  $O_2$  over the 10 wt%Ce-stabilized  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> supported 1 wt% Pd catalyst. Half cycle time, 20 s; reactant gas composition, (a) 0.3 vol% CO, 0.05 (reducing) and 0.2 (oxidizing) vol% O<sub>2</sub> with Ar tracer in He; (b) 0.05 vol% CH<sub>4</sub>, 0.05 (reducing) and 0.2 (oxidizing) vol% O<sub>2</sub> with Ar tracer in He; total flow, 100 cm<sup>3</sup>(NTP)/min; catalyst mass, 0.02 g; GHSV: 600000 h<sup>-1</sup>.

wt% Ce supported on LaAlO<sub>3</sub> also has poor oxygen storage performance (see Fig. 6a). Potential negative effect caused by presence of Pd can also be ruled out as LaAlO<sub>3</sub> supported 1 wt% Pd and 8 wt% Mn shows as good oxygen storage performance as LaAlO<sub>3</sub> supported MnO<sub>x</sub> alone.

TPO and TPR measurement results (not given) show that  $MnO_x$  has superior oxygen storage performance than ceria. Though the use of  $MnO_x$  is critically important for achieving good oxygen storage performance, supports also play very important roles. Among the supports we investigated,  $LaAlO_3$  and  $La_2O_3$ -stabilized  $Al_2O_3$  are the best.

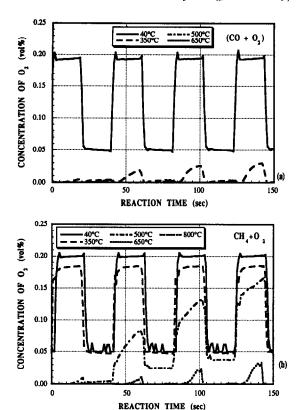


Fig. 6. Dynamic slow cycle redox reactions of CO and CH<sub>4</sub> with  $O_2$  over the LaAlO<sub>3</sub> supported 1 wt%Pd and 8 wt%Mn catalyst. Half cycle time, 20 s; reactant gas composition, (a) 0.3 vol% CO, 0.05 (reducing) and 0.2 (oxidizing) vol%  $O_2$  with Ar tracer in He; (b) 0.05 vol% CH<sub>4</sub>, 0.05 (reducing) and 0.2 (oxidizing) vol%  $O_2$  with Ar tracer in He; total flow, 100 cm<sup>3</sup>(NTP)/min; catalyst mass, 20 mg; GHSV: 600000 h<sup>-1</sup>.

The dynamic switched oxidation of CH<sub>4</sub> by  $O_2$  over 1 wt%Pd-10 wt%Ce/Al<sub>2</sub>O<sub>3</sub> and 1 wt%Pd-8%Mn/LaAlO<sub>3</sub> are given in Fig. 5b and Fig. 6b, respectively. Though, in terms of oxygen storage performance, 1 wt%Pd-10 wt%Ce/Al<sub>2</sub>O<sub>3</sub> is inferior to 1 wt%Pd-8%Mn/LaAlO<sub>3</sub> the catalytic activity of the former (not shown) is higher than the latter for oxidation of CH<sub>4</sub>. This difference cannot be the result of interaction between Pd and Ce because 1 wt%Pd-10 wt%Ce/LaAlO<sub>3</sub> has similar activity as 1 wt%Pd-8%Mn/LaAlO<sub>3</sub>. Thus, the high activity of ceria stabilized y-Al<sub>2</sub>O<sub>3</sub> supported Pd is the result of high dispersion of Pd on Al<sub>2</sub>O<sub>3</sub> which has a BET surface area of  $140\text{m}^2/\text{g}$  compared to  $16\text{ m}^2/\text{g}$  for LaAlO<sub>3</sub>. For this reason, we may prefer to have the catalytically active noble metal component supported on high surface area supports, for instance,  $LaAl_{11}O_{18}$  or  $La_2O_3$ -stabilized  $Al_2O_3$ . The high activity for  $CH_4$  oxidation and reforming to form  $NO_x$ -reducing CO and  $H_2$  shown by 1 wt%Pd-10 wt%Ce/ $Al_2O_3$  suggests the use of Pd-based catalyst can substantially reduce  $NO_x$  and  $CH_4$  emission in natural gas vehicles.

# 3.2. Physical mixtures of Mn/LaAlO<sub>3</sub> and Pd/LaAl<sub>11</sub>O<sub>18</sub> or Pt/CeO<sub>2</sub>/Al<sub>2</sub>O<sub>3</sub>

We have demonstrated that it is not necessary to support both the OSC component (MnO<sub>x</sub>) and noble metal on the same perovskite support. In fact, it is preferable to support the precious metal on a separate, stable, high surface area support, e.g. LaAl<sub>11</sub>O<sub>18</sub>, so that high dispersion of the metal component can be achieved. Based on this idea, we conducted dynamic cycle experiments with both (NO, <sup>13</sup>CO, and O<sub>2</sub>) and (NO,  $CH_4$ , and  $O_2$ ) simulated exhaust gas streams with a physical mixture of 10 mg 1 wt%Pt-8 wt%Mn/LaAlO<sub>3</sub> and 10 mg 1 wt%Pt-10 wt%Ce/Al<sub>2</sub>O<sub>3</sub>, and with a physical mixture of 10 mg 1 wt%Pt-8 wt%Mn/LaAlO3 and 10 mg 2wt%Pd/LaAl<sub>11</sub>O<sub>18</sub>. Previously, we found that calcination of LaAl<sub>11</sub>O<sub>18</sub> hexaaluminate supports at 1150°C for 72 h can ensure that these supports remained stable during methane combustion after repeated ( $\approx 100$ ) excursions to 950°C [11]. We have also examined the methane conversion activity of 1 and 2 wt% Pd and Pt catalysts supported on LaAl11O18 using temperature programmed techniques [11].

Results in Fig. 7(a) and Fig. 7(b) show that for NO reduction by CO, complete removal of  $O_2$  and complete reduction of NO are achieved at temperatures above 300°C. This beneficial effect must be the result of the combination of the greater activity of 1 wt%Pt-10%Ce/Al<sub>2</sub>O<sub>3</sub> with the greater oxygen storage capacity of the 1 wt%Pt-8 wt%Mn/LaAlO<sub>3</sub>. For NO reduction by CH<sub>4</sub>, complete removal of  $O_2$  and complete NO conversion are achieved  $\geq$  500°C.

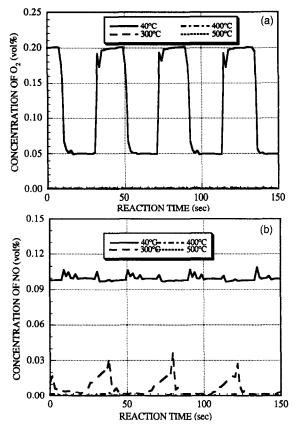


Fig. 7. Dynamic slow redox reaction of CO, NO, and  $O_2$  over physically mixed ceria (10 wt% Ce) stabilized  $Al_2O_3$  supported 1 wt% Pt and LaAlO<sub>3</sub> perovskite supported 1 wt% Pt and 8 wt% Mn catalyst at 40–800°C. Half cycle time, 20 s; reactant gas composition, 0.4 vol%  $^{13}$ CO, 0.1 vol% NO, and 0.05 (reducing) and 0.2 (oxidizing) vol%  $O_2$  with Ar tracer in He; total flow, 100 cm<sup>3</sup>(NTP)/min; catalyst mass, 50 mg each; GHSV: 240000h<sup>-1</sup>.

Similar beneficial effects are also observed for the physical mix of 1 wt%Pt-8 wt%Mn/LaAlO<sub>3</sub> and 2wt%Pd/LaAl<sub>11</sub>O<sub>18</sub> for

both NO reduction by CO and NO reduction by  $CH_4$ . Though addition of  $2wt\%Pd/LaAl_{11}O_{18}$  led to improved  $CH_4$  oxidation activity it is much less effective than 1 wt%Pt-10  $wt\%Ce/Al_2O_3$  despite both have high surface area. The superior performance of 1 wt%Pt-10  $wt\%Ce/Al_2O_3$  to 2  $wt\%Pd/LaAl_{11}O_{18}$  for NO reduction by  $CH_4$  may be due to higher surface area (141 vs. 95  $m^2$   $g^{-1}$ ) and deserves further investigation.

# 4. Durability of mixed three-way catalysts

Aging experiments were conducted on the physical mix of 1 wt%Pt-10 wt%Ce/Al<sub>2</sub>O<sub>3</sub> and 2 wt%Pd/LaAl<sub>11</sub>O<sub>18</sub> catalyst. This was done by heating repeatedly to 800°C and a single excursion to 950°C during reduction of NO by CO. We found that aging leads to some loss of oxygen storage capacity, and lower activity for NO reduction. However, the aged catalyst retains good activity for NO reduction and the conversion of NO is greater than 70% at  $\geq$ 500°C (Table 2). The loss of NO reduction activity was caused by decreasing surface area (sintering) not by the formation of complex Mn oxides. This demonstrates that our catalyst formulations not only give excellent performance for CH<sub>4</sub> oxidation and NO reduction but also can sustain good performance following a high temperature excursion to 950°C.

The above results demonstrate that noble metals are essential components in TWCs for

Table 2 Comparison of performance of a physical mixture of 1 wt%Pt-8 wt%Mn/LaAlO<sub>3</sub> and 2 wt%Pd/LaAl<sub>11</sub>O<sub>18</sub> for NO reduction by CO before and after ageing at 950°C for 30 min

Temperature	Fresh catalys	it .		Catalyst aged at 950°C		
(°C)	NO conversion (vol%)		OSC activity	NO conversion (vol%)		OSC activity
		O <sub>2</sub> -rich	$O_2$	CO-rich cycle	O <sub>2</sub> -rich cycle	${ m O_2}$ breakthrough
		cycle	breakthrough			
300	85	80	small	70	72	significant
400	98	90	small	85	80	significant
500	~ 100	82	very small	98	84	small
600	~ 100	80	very small	98	76	very small
700	~ 100	78	very small	98	74	very small

the reduction of NO<sub>x</sub> (mostly NO). When using CNG fuel, it is also very essential that the TWC convert some methane into reducing gases H<sub>2</sub> and CO to insure complete reduction of NO. While the supported manganese oxides show some activity for methane conversion, especially above 500°C, their activity under reducing conditions is low relative to the noble metals. Therefore, to be effective for NO<sub>x</sub> reduction using CNG fuels with lower CO and higher CH<sub>4</sub> levels in the engine exhaust gases, our manganese components for enhanced oxygen storage must be combined with a very active noble metal-based component. We anticipate either adding Pd or Pt to the MnO<sub>x</sub>/LaAlO<sub>3</sub> or adding supported noble metals as a separate phase for both NO reduction and the production of reducing gas.

# 5. Conclusions

MnO<sub>x</sub> supported on LaAlO<sub>3</sub> perovskite is superior to ceria in several ways: (i) it directly and rapidly absorbs oxygen without need for noble metals to promote the rate of oxygen absorption; (ii) it exhibits a larger capacity for oxygen storage over a wide temperature range; (iii) it directly oxidizes CH<sub>4</sub>; and (iv) with assistance of noble metals, it shows steam reforming or partial oxidation activity (converting CH<sub>4</sub> and steam into CO and H<sub>2</sub>). This ability to

generate CO and  $H_2$  under oxidizing conditions is especially important for reducing  $NO_x$  emissions in NGV exhaust gas.

# Acknowledgements

This work was funded by the United States Department of Energy under its SBIR Program and supported by Goremotive Industries, Inc.

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